

FORMING ANALYSIS OF CONTINUOUSLY ANNEALED, DOUBLE REDUCED STEEL SHEETS

Emil Spišák¹, Janka Majerníková¹, Peter Mulidrán¹, Ľuboš Kaščák¹, Ján Slota¹

¹ Technical University of Košice, Faculty of Mechanical Engineering, Mäsiarska 74, 040 01 Košice, Slovakia, e-mail: emil.spisak@tuke.sk, janka.majernikova@tuke.sk, peter.mulidran@tuke.sk, lubos.kascak@tuke.sk, jan.slota@tuke.sk

Received: 2018.06.27
Accepted: 2018.08.01
Published: 2018.09.01

ABSTRACT

The paper deals with the forming analysis of continuously annealed steel sheets double reduced. Six different metal sheet grades were evaluated in the paper, thickness was in the range from 0.15 to 0.175 mm. Described are the used methods and the results obtained by a uniaxial tensile test, biaxial test (bulge test) and a springback test.

Keywords: forming analysis, springback, packaging steel.

INTRODUCTION

The production of thin sheets has undergone significant changes over the years. These changes include, in particular, a significant change in the thickness of the packaging sheets from the original thickness from 0.24–0.22 mm to a thickness of 0.14–0.16 mm. These thicknesses are achieved by introducing a second reduction. In the case of such packaging sheets, higher strength properties, in particular the Yield strength, are achieved with sufficient (for further processing by forming) plastic properties. In view of the significant changes in production of packaging steel sheets and the increasing requirements for determining their properties, it is also necessary in the area of their evaluation to seek objective, rapid and cost-effective test methods to determine their mechanical and plastic properties. Due to the fact that many different methods of mechanical properties evaluation are used by the sheet metal manufacturers and processors, the results of the mechanical properties determined by the uniaxial test, the biaxial test (bulge test) and the springback test are compared in this paper. In the paper, sheets produced by the second reduction, continuously annealed will be compared.

The results should lead to the optimization of the test method for determining the objective mechani-

cal properties of the sheets and thus to create the conditions for their trouble-free processing by drawing.

MATERIALS USED IN EXPERIMENT

For experimental research of the formability of continuously annealed sheets, continuous annealed materials of different thicknesses and different melts were used. In total, 6 types of two kinds of TH 550 CA, TH 620 CA sheets, 0.15 to 0.175 mm thickness (Table 1) were used.

UNIAXIAL TENSILE TEST

It is currently the most widely used test that acquires the basic mechanical properties of the sheet metal. The test conditions and shape

Table 1. Materials used in experiment

Material	Sample thickness [mm]	Sample number
TH 550 CA	0.155	47
	0.17	1
	0.175	83
TH 620 CA	0.152	90
	0.17	48
	0.175	69

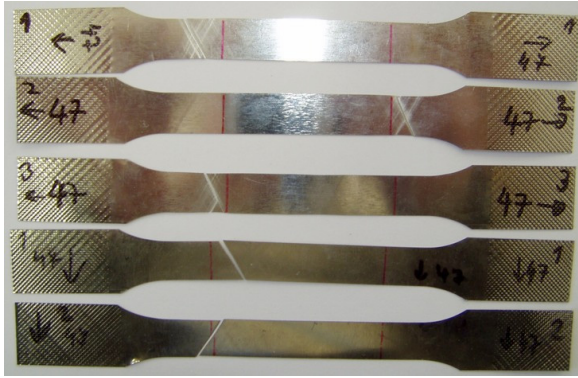


Fig. 1. Specimen after uniaxial tensile test, tested material was TH 550 CA, thickness of the material was 0.155 mm

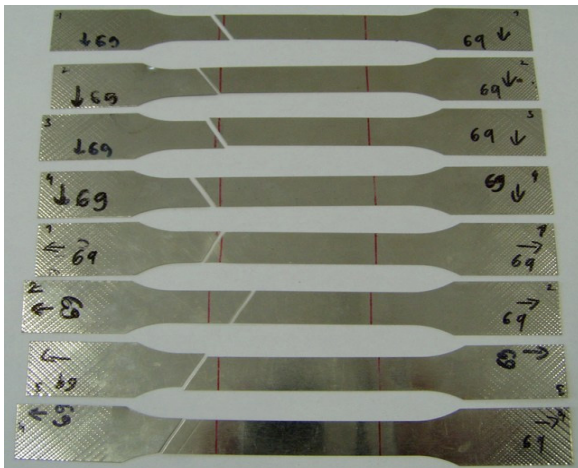


Fig. 2. Specimen after uniaxial tensile test, tested material was TH 620 CA, thickness of the material was 0.175 mm

of the test specimen are specified in STN EN 10002-1 + AC1 and STN 42 0321. For tinsteel sheets we often determine the Ultimate tensile strength, Yield strength and ductility of the material. These properties are obtained from uniaxial tensile test. To assess the anisotropic properties of the material, samples were taken in a 0° and 90° direction relative to the rolling direction for the tensile test.

In Fig. 1 samples of class TH 550 CA and in Fig. 2 are samples of the class TH 620 CA are presented, both after the uniaxial tensile test. For both of these steels, almost all the samples taken in the rolling direction also samples taken in a direction perpendicular to the rolling direction fractured outside the measured section. The slip spread approximately at an angle of 45°.

BIAXIAL TENSILE TEST – BULGE TEST

Biaxial tension is one of the most unfavorable types of stress schemes in plastic deformation of steel sheets. That is the reason, why it is suitable to use this type of stress for determination of plastic and mechanical properties of steel sheets. Biaxial hydraulic tensile test, also known as Bulge test is very good for resembling biaxial tension. Fundamentals of this test are shown in Fig. 3.

Measured signals from specimen height sensor and from fluid pressure sensor are processed by technological card and by our own software in graph „stress – strain“. The record obtained from testing equipment is shown in Fig. 4.,

Biaxial tensile test is based on bulging sheet metal by hydraulic fluid under pressure. Tested sheet is held between bottom plate and die with radius of 40 mm. It is possible to regulate blank holding force by the valve. Specimen flange prevents drawing of the material with the use of bead, which is located in die. Sheet metal is bulged by

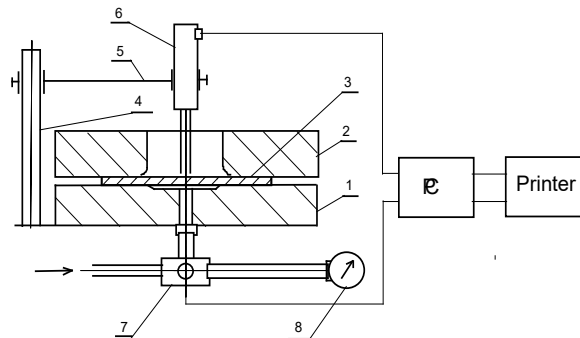


Fig. 3. Principal scheme of Bulge test

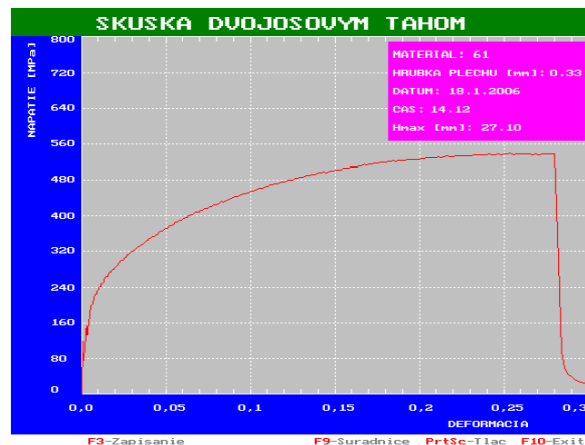


Fig. 4. Graph „Stress – Strain“ obtained from bulge test

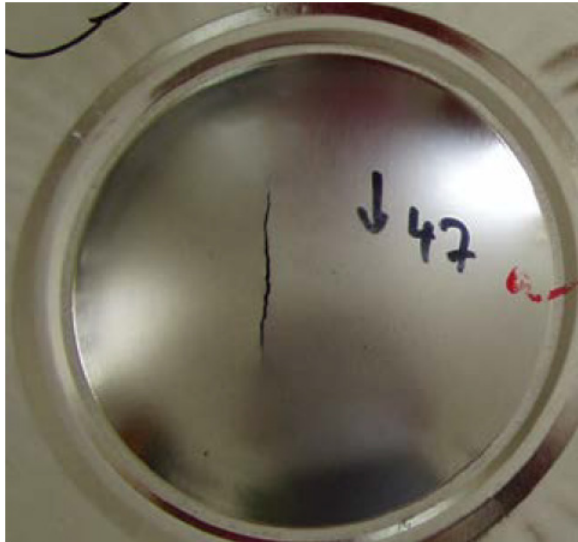


Fig. 5. Specimen N.47 after bulge test, tested material was TH 550 CA, with thickness of 0.155 mm

the pressurized hydraulic fluid until specimen is fractured. The height of the fractured bulged specimen, shape of fracture and surface of specimen after fracture is evaluated in this test.

For this test, square specimens with dimension of 130x130 mm were used. Materials were the same as in the uniaxial tensile test (Fig. 5 and Fig 6). From the test, Yield Strength R_e , Ultimate tensile strength R_m , bulge height and overall strain was evaluated.

SPRINGBACK TEST

This test was developed for the purpose of simple determination of the Yield strength of tinsteel sheets while characterizing its certain plastic properties. The test is based on the theoretical basis of elastic and plastic deformation and uses one of the basic laws of the metal forming theory, the law of the presence of elastic deformation at each plastic deformation. The Yield strength values were based on the table recommended by the device manufacturer depending on the springback angle.

A sample of 152.4 x 25.4 mm is used to perform the test, which is clamped at one end and the second free end is bent to 180 ° about a 25.4 mm diameter mandrel by means of a roller. The roller returns to the starting position and the springback angle is read off directly on the scale.

Amount of curvature is defined by:

$$\theta/180^\circ = 1 - (r_0 - r_1) \quad (1)$$

where: θ – springback angle [°]; r_0 – radius of mandrel [mm]; r_1 – radius of specimen after springback [mm].

Relationship between θ and R_e is defined by:

$$\theta/180^\circ = 3[(R_e \cdot r)/(E \cdot t)] - 4[(R_e \cdot r)/(E \cdot t)]^3 \quad (2)$$

where: R_e – Yield Strength [MPa], E – Young’s modulus [MPa], θ – Springback angle [mm], r – Bending radius [mm], t – Thickness of specimen [mm].

RESULTS

Measured results of strength and plastic properties of continuously annealed packaging sheets are shown in Fig 7., 8. and 9. In Fig. 7 the values of Yield strength obtained by uniaxial tensile test, biaxial tensile test (bulge test) and springback test are compared.

It follows from the figure that the measured values of the tensile strength obtained by the uniaxial tensile test for the TH 550 CA grade material are in all samples taken in the rolling direction and in the samples taken in a direction perpendicular to the direction of rolling within the limits of the values recommended by the relevant standard (only specimen N. 47 shown value out of standards limits). For TH 620 CA grade steel, the values of Yield strength obtained by the uniaxial tensile test for all measured samples taken in the rolling direction and in a direction perpendicular to the direction of rolling were in the tolerance specified by the relevant standard.

Values of Yield strength obtained from biaxial tensile test for TH 550 CA grade steel were in the



Fig. 6. Tested material TH 620 CA, with thickness of 0.175 mm after bulge test

tolerance specified by the relevant standard, but values of Yield strength for material TH 620 CA were not in the tolerance specified by the standard. Values of Yield strength obtained from Springback test were within limit of standard for TH 620 CA steel. For TH 550 CA steel, values of Yield strength were over the limit specified by the standard.

In Fig. 8, the values of tensile strength obtained in the uniaxial tensile test and the biaxial tensile test is compared. The measured values in the uniaxial tensile test and values obtained by the biaxial tensile test were within the limits specified by the relevant standard.

A comparison of the ductility of the investigated packaging steel sheets is shown in Fig. 9. It is evident from the figure that the highest values of ductility for both grades were achieved in the biaxial test (except for sample N. 1).

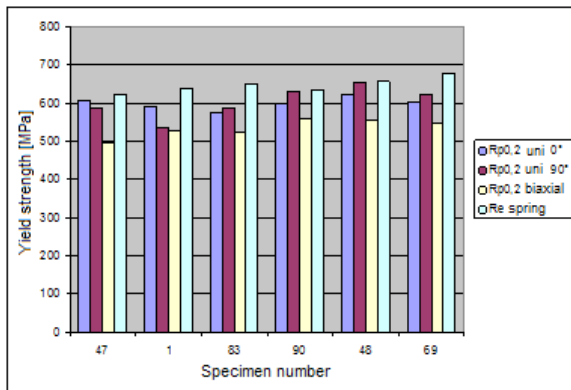


Fig. 7. Comparison of the Yield strength obtained in the uniaxial test in a 0° and 90° direction, the Yield strength obtained by the biaxial tensile test and the Yield strength obtained by the springback test

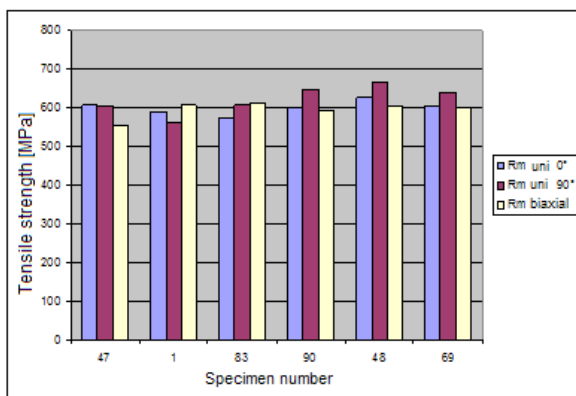


Fig. 8. Comparison of the tensile strength obtained in the uniaxial test in a 0° and 90° direction and tensile strength obtained by the biaxial tensile test

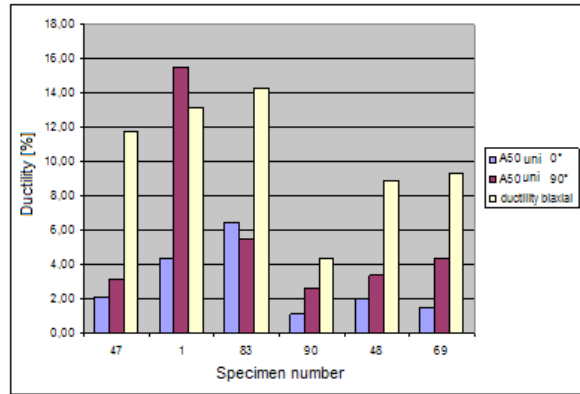


Fig. 9. Comparison of the A50 ductility obtained in the uniaxial test in a 0° and 90° direction and the “ductility” obtained in the biaxial tensile test

CONCLUSIONS

Based on the experiments, it can be concluded that the strength and plastic properties of the thin packaging sheets determined by the different tests cannot be compared.

The results of the uniaxial tensile test achieve the closest values for Yield strength and tensile strength in terms of the results set by the standard. The ductility values obtained from this test achieve considerable scattering, which is caused, in particular, by fracturing of the samples out of the measured area and locating the plastic deformation without developing the deformation over the entire measuring range.

The Yield strength is lower in the biaxial pull test for all investigated materials than in the uniaxial pull test. This is due to the strain – biaxial tensile stress.

In the springback test, the Yield strength values were the highest. This may be due to an inappropriate mathematical model for determining the Yield strength for these steel sheet grades. For further use of this test, it is necessary to review models for calculating the Yield strength.

Acknowledgements

The authors are grateful to APVV for support of experimental work under grant APVV-14-0834 and the project VEGA No. 1/0441/17.

REFERENCES

1. Spišák, E., Slotá, J., Majerníková, J.: Hodnotenie anizotropie tenkých obalových plechov. In: Visník: Naukovo-mechničnij zbornik. Kijev: Nacionalnij transportnij univrsitet, 2006, p. 23-29.

2. Majerníková, J.: Medzné deformácie tenkých obalových plechov pri rôznych napätovo-deformačných stavoch. Dizertačná práca, Košice, 2008.
3. Spišák, E. – Majerníková, J: Properties evaluation of progressive wrapping materials. In: Mechanical Engineering SI 2008: 12th International Conference: proceedings of papers. Bratislava STU, 2008. ISBN 978-80-227-2982-6. S. 1-8.
4. Spišák, E., Slota, J., Majerníková, J.: Analýza začiatku plastickej deformácie DR obalových plechov. In: Acta Mechanica Slovaca. roč. 10, č. 2b Pro-tech-ma (2006), s. 387-392. ISSN 1335-2393.
5. Spišák, E. – Majerníková, J.: Plastic deformation of tin coated steel sheet under different stress-strain states. In: Progressive technologies and materials. 3-B : Materials. Rzeszów : Oficyna Wydawnica Politechniki Rzeszowskiej, 2009. ISBN 978- 83-7199-550-7. - P. 25-35.
6. Chongthairungruang, B; Uthaisangsuk, V. Springback prediction in sheet metal forming of high strength steels, *Materials and Design* 2013, 50, pp. 253-266. 10.1016/j.matdes.2013.02.060.
7. Lei, D; Xinyun, W; Junsong, J; Liangjun, X. Springback and hardness of aluminum alloy sheet part manufactured by warm forming processs using non-isothermal dies, *Procedia Engineering* 2017, 207, pp. 2388-2393. 10.1016/j.proeng.2017.10.1013.
8. Wagoner, R; H. Lim, H; Lee, M.G.. Advanced Issues in springback, *International Journal of Plasticity* 2013, 45, pp. 3–20. <https://doi.org/10.1016/j.ijplas.2012.08.006>.
9. Trzepiecinski, T; Lemu, H, G. Effect of Computational Parameters on Springback Prediction by Numerical Simulation, *Metals* 2017, 7, pp. 380. 10.3390/met7090380.
10. Mulidran, P; Spisak, E; Majernikova, J; Sleziak, T; Gres, M. Influence of forming method and process conditions on springback effect in the sheet metal forming simulation, *International Journal of Engineering and Science (IJES)* 2017, 6, pp. 62-67. 10.9790/1813-0612016267.
11. Banabic, D. Advanced anisotropic yield criteria. In *Sheet Metal Forming Processes*, 1st edition; Springer Heidelberg Dordrecht, Berlin, Germany, 2010, pp. 76-87, ISBN 978-3-540-88112-4.
12. Jung, J, B; Jun, S; Lee, H,S; Kim, B,M; Lee, M,G; Kim, J,H. Anisotropic Hardening Behaviour and Springback of Advanced High-Strength Steels, *Metals* 2017, 7, pp. 480. 10.3390/met7110480.
13. Banu M, Takamura M, Hama T, Naidim O, Teodosiu C, Makinouchi A. Simulation of springback and wrinkling in stamping of a dual phase steel rail-shaped part, *J Mater Process Technol* 2006, pp. 173-178. 10.1016/j.jmatprotec.2005.11.023.
14. Slota, J; Spisak, E. Comparison of the forming-limit diafram (FLD) models for drawing quality (DQ) steel sheets, *Metalurgija* 44 2005, 4, pp. 249-253.