INTRODUCTION

The comfort of a car is assessed in various ways, such as according to the softness of a seat, the type of the body, automatic or mechanical gearbox, electronic devices and so on. However, the key criteria for choosing a comfortable vehicle should be the absorption of the road inequalities, an intensity of the sensible vibrations and a perceptibility of the vehicle body oscillations.

Drivers or passengers of vehicles do not wish to feel any additional vibrations caused by the road irregularities. Comfort influences the psychological thinking of a person as well. If driving is comfortable, a person is calm and duly concentrates their attention on driving the vehicle. Vibrations are the oscillations with amplitude that is considerably lesser than the geometrical parameters of the oscillating object. This physical phenomenon may predetermine the mood and emotional outbursts of a person, so the influence of the vehicle suspension characteristics on the driving comfort was assessed herein.

THE INFLUENCE OF SEMI-ACTIVE SUSPENSION ON DRIVING COMFORT

The vehicle suspension reduces the influence of the road inequalities transferred to the vehicle body while driving on the roads of various levels of quality. Therefore, the shock absorbing and damping characteristics of suspensions should ensure safe and comfortable conditions for the transportation of passengers. While analysing the operation of a vehicle suspension, a certain assessment criterion that would define the quality of the suspensions and enable comparing various versions, is required. Meanwhile, no uniform parameter that would fully characterise the vehicle movement softness is accepted. The usable assessment criteria include the displacement...
velocity, acceleration, body oscillations and so on. The problem of criterion choosing is intractable because the task of describing the influence of vibrations on a human body by a single parameter is complicated [1, 9, 14, 16].

While describing the interaction between a human body and a source of vibrations, the system of coordinates ISO 2631–1 [5] with its origin in zone of the human heart was used. The directions of the axes of coordinates conform to the stance of the person (Fig. 1). Establishing such a position of the point of origin of coordinates is rather difficult; in addition, provision of a precise description of the place where the oscillations should be measured is a complicated task as well. For a more precise analysis, the oscillations that affect the main parts of the human body were assessed, i.e. individual points of origin of coordinates were established in the principal points between the vibrating surface and the relevant part of the body. In such a case, the following points of origin of coordinates are foreseen for a sitting person: on the seat, in the point of the support of the feet and in the point of support of the back [4].

The problem of passengers’ comfort sensation in modern vehicles was discussed up by Dertimanis et al. In the study, the passive (Fig. 2) and active (Fig. 3) types of suspension systems as well as their influence on the travelling comfort were described [3].

In their studies, many researchers analysed: the response of the vehicle suspension to the road inequalities dependent on the vehicle wheelbase, the changes in the vehicle velocity dependent on the road surface, the passenger’s comfort sensation on different vibrations of the suspension caused by the road inequalities as well as different stiffness and dampness characteristics [2, 7, 11, 17]. The method accomplishing the test includes establishing the coefficients of displacement between the rear axle and the front axle as well as the average values of the displacement between the rear axle and the front axle. Then, the road profiles (sinusoidal, highway or an urban street) are chosen. The coefficients of displacement between the rear axle and the front axle as well as the averages of the coefficients of displacement between the rear axle and the front axle are inserted in the motion equation. According to the obtained displacements, the diagrams of oscillations

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**Fig. 1.** The system of coordinates usable for assessing the vibrations that affect a human body [5]

**Fig. 2.** A kinematic model of a passive suspension [3]
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and accelerations are formed. The obtained results were compared to the values presented in the provisions of the ISO 1520 standard [13].

The ride comfort of a vehicle equipped with a semi-active suspension may be established according to the automatic suspension versions setting inside the vehicle. Žuraulis et al. carried out the tests on modern vehicles in “Comfort” and “Sport” suspension control modes. The benefit gained by the driver, when two different modes of driving are used, was analysed in the article. In the tests, two E class vehicles “Mercedes Benz” and “Opel Insignia” were involved. They are vehicles of quite different types. They were used for driving on two different 350 m long fragments of a motorway at different velocities: 30, 50, 70 and 100 km/h. During the experiment, the suspension settings were varied, whereas on movement with different velocities and on different road surfaces, the vertical acceleration in the zone of the passenger’s seat was fixed. For the test, a “Corrsys-Datron DAS-3” accelerometer, one of the key devices usable for travel comfort assessing, was used. In the course of varying the settings of the suspension and the whole chassis during the experiment, it was found that vibration affecting the passenger (the passenger’s vibration dose value) is lower at lower driving velocities (30 or 50 km/h). At higher velocities, the amplitudes of the vibrations increase; in the “Sport” mode, the amplitudes of vibrations were lower, as compared to “Comfort” mode. On movement upon “Comfort” mode, the vehicle body was prone to vibrations of higher intensity [18, 19].

In the paper by Wang et al., the higher support of the shock absorber (a mechanical element of a vehicle suspension), otherwise referred to as a shock damper, was analysed. The scientists had raised the question, whether a small detail intended to accept and mitigate the shocks from the shock absorber is able to influence the travelling comfort. The experiments were accomplished by driving on uneven roads, including protruding islands, corrugations and so on. During the experiment, it was proven to be important for the ride comfort, because a larger share of a shock absorbed by the shock absorber causes lower amplitudes of the vibrations transferred to the body. While driving on protruding bumps, the absorbing materials of the relevant height and softness were chosen. Shock absorbers only move the body to the relevant direction; however, they do not transfer vibrations and oscillations to the driver’s and passenger’s seats [15].

In terms of braking and accelerating, the principle applicable for driving on bumps is applied as well: on braking, the front shock dampers pull the shock absorber arm to the lower position, whereas while accelerating – the rear shock dampers press the shock absorber. The scientists tested this theory on several different models of vehicles; however, one negative factor had been observed: an attrition of shock dampers is much faster, because they are softer [10, 12, 15].
The key parameters of lateral dynamics include:
• lateral acceleration;
• roll rate;
• body tilt angle in respect of longitudinal axis;
• projection of the roll rate;
• projection of the pitch rate;
• side-slip angle;
• yaw rate.

THE METHODOLOGY OF THE EXPERIMENTAL RESEARCH

During the experimental research, a sinusoidal manoeuvre was carried out: the vehicle was moving with constant velocity of 40 km/h and its steering wheel was rotated at a certain angle on a certain moment. The type of the manoeuvre and the steering wheel rotating angle are shown in Fig. 4 below.

The conditions for an accomplishment of the experimental research:
• The vehicle under the research: “Mercedes Benz E” car.
• The equipment of the vehicle under the research is intended for measuring the vehicle body displacements and the accelerations in the lateral and vertical direction.
• Rotation of the vehicle steering wheel is controlled by the installed robot; the robot, in turn, is controlled via a controlling code programmed by “Arduino” software.
• The tests were carried while driving on asphalt pavement upon three different suspension control modes (the mode I – the minimum height of the body over the ground; the mode II – the middle height of the body over the ground; the mode III – the maximum height of the body over the ground (the measurement is performed between the road surface and the lowest point of the front and rear wing arc at the wheel centre) and different sizes of wheels: 225/55 R16 (hereinafter – 16”) and 245/45 R17 (hereinafter – 17”). The impact of different suspension modes on the distance between the body and the road surface is shown in Table 1 below.

Upon striving to avoid considerable errors and those caused by the human factor during the accomplishment of the manoeuvre, a rotating robot

Table 1. The distance of the vehicle from the road surface upon different suspension control mode

<table>
<thead>
<tr>
<th>Wheel size</th>
<th>Mode</th>
<th>Front axle, m</th>
<th>Rear axle, m</th>
</tr>
</thead>
<tbody>
<tr>
<td>225/55 R16</td>
<td>Mode I</td>
<td>0.677</td>
<td>0.685</td>
</tr>
<tr>
<td></td>
<td>Mode II</td>
<td>0.670</td>
<td>0.673</td>
</tr>
<tr>
<td></td>
<td>Mode III</td>
<td>0.720</td>
<td>0.728</td>
</tr>
<tr>
<td>245/45 R17</td>
<td>Mode I</td>
<td>0.688</td>
<td>0.696</td>
</tr>
<tr>
<td></td>
<td>Mode II</td>
<td>0.680</td>
<td>0.686</td>
</tr>
<tr>
<td></td>
<td>Mode III</td>
<td>0.731</td>
<td>0.740</td>
</tr>
</tbody>
</table>

![Fig. 4. The type of manoeuvre and the steering wheel rotating angle](image)
had been fixed on the steering wheel (Fig. 5). The said robot is controlled by “Arduino” software where a programming code for the robot controlling was developed.

The robot for the steering wheel rotation control is, in turn, controlled upon applying “Arduino” software. In the programming window, the key parameters of the sinusoidal movement foreseen for the experiment are shown: the rotation angle of the steering wheel – 80°, the time interval between its rotating actions – 1 second, the rate of the steering wheel rotation – 2π/s, the reduction gear ratio – 3.64, the number of segments of the manoeuvre – 5.

THE RESULTS OF THE EXPERIMENTAL RESEARCH AND THEIR ANALYSIS

During the experiments, the total information obtained by the sensors was fixed; however, more attention was paid to observing the body tilt angle and the lateral acceleration. In order to establish the maximum values of the said parameters as well as their distribution and changes, the results of the experiments and their comparison were presented in diagrams (Figs. 6 and 7).

The summarised results of the experimental research are provided in Table 2 below.

Fig. 5. The robot for controlling the steering wheel turning used in the experimental research

Fig. 6. Fluctuations of the lateral acceleration for different heights of the vehicle body
The maximum lateral acceleration (3.67 m/s²) was fixed for driving in mode I, with 16” wheels, and the maximum body tilt angle (7.8º) was fixed for driving in mode II, with 16” wheels. The minimum lateral acceleration (3.02 m/s²) was fixed for driving in mode III, with 17” wheels and the minimum body tilt angle (6.05º) – for in II and 17” wheels.

Root mean square (RMS) m/s² shall be calculated as follows [6]:

\[ RMS = \left( \frac{1}{T} \int_0^T a_w^2(t) \, dt \right)^{\frac{1}{2}} \]  

(1)

where: T – duration of measurement (integration) (s);
\( a_w(t) \) – instantaneous weighted value of the vibration acceleration on the moment \( t \) in the direction of vertical axis (m/s²).

The weighted value of vibration acceleration \( a_w(t) \) (m/s²) defines the different impact of frequency on the response of human body to vibration and is expressed as follows [8]:

\[ a_w(t) = \left( \sum_n W_n \cdot a_n \right)^2 \] 

where: \( W_n \) – weighting factor applicable to the \( n \)-th frequency range;
\( a_n \) – the measured root mean square (RMS) of the vibration acceleration in the \( n \)-th frequency range (m/s²).

For a primary evaluation of a passenger’s comfort sensation, the methodology described in the ISO 2631–1 international standard [5] was chosen. According to the said methodology, the root mean square (RMS) was established. The calculations showed more considerable impact of the “Comfort” mode for speeds up to 50 km/h only. Higher differences between the values established for the “Comfort” and “Sport” modes were found for driving on asphalt pavement fragment with considerable road inequalities.

If the values of vertical accelerations caused by road inequalities are transferred from the time domain to the frequency domain, it becomes possible to assess the amplitudes of the accelerations

**Table 2. Comparison of values of the lateral acceleration and the body tilt angle**

<table>
<thead>
<tr>
<th>Test</th>
<th>Lateral acceleration, (m/s²)</th>
<th>Body tilt angle (in respect of longitudinal axis), (°)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Maximum</td>
<td>Average</td>
</tr>
<tr>
<td>Mode I, 16”</td>
<td>3.67</td>
<td>2.88</td>
</tr>
<tr>
<td>Mode II, 16”</td>
<td>3.36</td>
<td>2.51</td>
</tr>
<tr>
<td>Mode III, 16”</td>
<td>3.24</td>
<td>2.34</td>
</tr>
<tr>
<td>Mode I, 17”</td>
<td>3.49</td>
<td>2.62</td>
</tr>
<tr>
<td>Mode II, 17”</td>
<td>3.29</td>
<td>2.44</td>
</tr>
<tr>
<td>Mode III, 17”</td>
<td>3.02</td>
<td>2.21</td>
</tr>
</tbody>
</table>
affecting the passenger more objectively. At the minimum velocity, the “Sport” mode caused higher accelerations, as compared to the “Comfort” mode; however, on increasing the velocity, the changes of the results were contrary. At higher velocities, higher limits of affected acceleration were achieved in the “Comfort” mode. This result does not mean that the “Comfort” mode does not cause any additional sense of comfort. It was found that the maximum values of acceleration both in the “Sport” and “Comfort” mode take place at the frequency of 1.5 Hz, so it may be stated that the “Comfort” mode causes a higher sense of comfort, as compared to the “Sport” mode: the intensity of vibrations is the same, only the amplitudes are higher in the first case, i.e. in the “Comfort” mode.

CONCLUSIONS

- In the course of the experimental research, it was found that the maximum lateral acceleration of the vehicle is 3.67 m/s² (on driving upon the mode I with 16” wheels), and the minimum lateral acceleration is 3.02 m/s² (on driving upon the mode III with 17” wheels). The manufacturer points out that upon the latter suspension control mode, the velocity should not exceed 45 km/h, because the said mode is not applicable to higher velocities (they may cause too intensive vibrations of the body which, in turn, may reduce the grip of tyres on the road.
- While comparing the differences between the values of lateral acceleration of the vehicle body obtained in course of the experimental research for different suspension modes, it was found that the maximum difference (21.5%) was fixed between the mode I with 16” wheels and the mode III with 17” wheels, and the minimum difference (1.5%) – between the mode III with 16” wheels and the mode II with 17” wheels.
- The difference between the maximum and minimum values of body tilt angle about the longitudinal axis found during the experimental research was 1.63°, or 30%.
- While comparing the impact of the wheel size on the lateral acceleration of the body, it was found that the minimum impact was caused on driving in mode II with 16” and 17” wheels (2.1 %) and the maximum impact – on driving in mode III with 16” and 17” wheels (7.28 %).
- Similar modern-day semi-active suspension systems with different suspension-driving options show that even the “Comfort” mode can act as a sporty, stiff suspension in order to keep up with road irregularities and suppress the vertical occupant seat accelerations, hence maintaining optimal tire-road contact and ensuring traffic safety.

REFERENCES


